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Protective clothing for firefighters – Physiological impact – Part 2: Determination of physiological heat load caused by protective clothing worn by firefighters (ISO 18640-2:2018)

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EUROPEAN STANDARD

EN ISO 18640-2

NORME EUROPÉENNE

EUROPÄISCHE NORM

May 2018

ICS 13.340.10

English Version

Protective clothing for firefighters - Physiological
impact - Part 2: Determination of physiological heat
load caused by protective clothing worn by firefighters
(ISO 18640-2:2018)

Vêtements de protection pour sapeurs-pompiers
- Impact physiologique - Partie 2: Détermination
de la déperdition de chaleur provoquée par
les vêtements de protection portés par les
sapeurs-pompiers (ISO 18640-2:2018)

Schutzkleidung für die Feuerwehr - Physiologische
Wärmebelastung - Teil 2: Bestimmung der
physiologischen Wärmebelastung ausgelöst
durch von Feuerwehrleuten getragene
Schutzkleidung (ISO 18640-2:2018)

This European Standard was approved by CEN on 2 January 2018.

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COMITÉ EUROPÉEN DE NORMALISATION
EUROPÄISCHES KOMITEE FÜR NORMUNG

CEN-CENELEC Management Centre: Avenue Marnix 17, B-1000 Brussels

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European foreword

This document (EN ISO 18640-2:2018) has been prepared by Technical Committee ISO/TC 94 "Personal safety - Personal protective equipment" in collaboration with Technical Committee CEN/TC 162 "Protective clothing including hand and arm protection and lifejackets" the secretariat of which is held by DIN.

This European Standard shall be given the status of a national standard, either by publication of an identical text or by endorsement, at the latest by November 2018, and conflicting national standards shall be withdrawn at the latest by November 2018.

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The text of ISO 18640-2:2018 has been approved by CEN as EN ISO 18640-2:2018 without any modification.

Introduction

Protective clothing for (structural) firefighting may have a serious physiological impact^{1),2)} on the wearer and a serious effect on the acute physical condition of the wearer during activities with increased metabolic heat production^{[3][4]}. Protective clothing impedes heat exchange by sweat evaporation and therefore maintenance of a constant core body temperature and thermal homeostasis is disturbed. This could increase the risk of heat strain and subsequently impact on the length and time that the firefighter is able to work safely. If this is identified in a risk assessment, it is important that (thermal) physiological parameters are obtained to ensure the suitability of the protective clothing chosen under the expected conditions of use. The assessment of the physiological impact of the protective clothing provides important information about the effect on individuals undertaking different tasks in various environmental conditions. In ISO 18640-1, relevant physical parameters of protective clothing are measured with a Sweating torso. Standard Sweating torso measurements provide physical parameters about combined and complex heat and moisture transfer (ISO 18640-1). By coupling the sweating torso to a mathematical model for thermo-physiological responses, the thermo-physiological impact of protective clothing is estimated and the maximum exposure time for defined environmental conditions and a defined activity protocol are predicted by Thermal Human Simulator (THS) measurements.

The purpose of this document is to consider aspects of protective clothing performance that cannot be determined by tests described in other standards. The aim of this document is to quantify the thermo-physiological impact of protective garments for (structural) firefighting under relevant exposures. This document provides the background for the specification of a minimum level of performance requirements during defined firefighting scenarios for the assessed firefighters' protective clothing by calculation of the maximum allowable work duration in order to avoid heat stroke.

NOTE The method allows to characterizing the thermo-physiological impact for different levels of complexity. This includes the characterisation of the single PPE ensembles (standard procedure) as well as the characterisation of protective clothing ensembles including under wear and protective clothing, including air layers or including design features of protective clothing ensembles (e.g. pockets, reflective strips) as optional procedures³⁾.

1) Nunneley (1989) reported a significant physiological burden due to the protective clothing upon the wearer, both in the form of increased metabolic rate and reduced heat dissipation.

2) Taylor (2012) showed that the relative influence of the clothing on oxygen cost was at least three times that of the breathing apparatus.

3) This listing of standard and optional procedures is a first proposal for prioritization. The expressiveness of the different levels of complexity for the characterisation of the thermo-physiological impact needs to be further investigated. Results will be presented at the next ballot.

Protective clothing for firefighters — Physiological impact —

Part 2:

Determination of physiological heat load caused by protective clothing worn by firefighters

1 Scope

This document specifies a method for evaluating the thermo-physiological impact of protective fabric ensembles and potentially protective clothing ensembles in a simulated activity under defined relevant conditions for firefighters.

This document is intended to be used to assess the thermo-physiological impact of protective fabric ensembles and potentially protective clothing ensembles but not the risk for heat stress due to actual fire conditions. The results of this test method can be used as elements of characterisation and comparison of thermo-physiological impact of various types of protective fabric ensembles and potentially protective clothing ensembles.

Default measurements are undertaken on fabric samples representing the garment or protective clothing combination. Optionally and in addition to the standard test method, the same testing protocol can be applied to characterise protective clothing ensembles including underwear, air layers and certain design features¹⁾. In addition measurements on readymade garments are optionally possible.

NOTE The presently used evaluation methods are only validated for structural firefighting garments.

2 Normative references

The following documents are referred to in the text in such a way that some or all of their content constitutes requirements of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO 11092, *Textiles — Physiological effects — Measurement of thermal and water-vapour resistance under steady-state conditions (sweating guarded-hotplate test)*

ISO 18640-1, *Protective clothing for firefighters-physiological impact — Part 1: Measurement of coupled heat and mass transfer with the sweating torso*

3 Terms and definitions

For the purposes of this document, the terms and definitions given in ISO 18640-1 and the following apply.

ISO and IEC maintain terminological databases for use in standardization at the following addresses:

- ISO Online browsing platform: available at <https://www.iso.org/obp>
- IEC Electropedia: available at <http://www.electropedia.org/>

1) A study conducted at Empa (Swiss Federal Laboratories for Materials Science and Technology, Switzerland) showed good correlation between results of standard torso tests (without both underwear and air layers on fabrics) to tests on fabrics with underwear, tests on fabrics with underwear and air layers and test on readymade garments (with underwear and with or without air layers) of the same material composition. Due to the different thermal insulation of the systems direct comparison of the results is not possible.

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3.1 core body temperature

T_{co}
temperature of deep body tissues of the human body

3.2
firefighting scenario
set of environmental conditions, a defined workload and a defined exposure time relevant for a firefighters' task

3.3
heart rate
number of heartbeats per unit of time

Note 1 to entry: The heart rate is usually expressed in per minute.

3.4
heat storage
heat accumulation in the body affected by metabolic heat produced, external heat load and heat dissipated from the body

3.5
maximum allowable work duration
MAWD
value calculated from thermo-physiological simulation (THS measurement) predicting the time to reach heat stress based on the definitions of this document

Note 1 to entry: See also [Annex A](#).

Note 2 to entry: This value is given in minutes.

3.6
mean skin temperature
 $T_{m,sk}$
mean temperature of the outer surface of the (human) body measured at several locations of the skin

3.7
skin diffusion
 E_{sk}
evaporative heat loss due to insensible skin perspiration and has to be provided for THS measurements

3.8
sweating torso
upright standing cylindrical test apparatus, simulating the human trunk with thermal guards on the upper and lower end as defined in ISO 18640-1

3.9
sweat rate
amount of moisture perspired per time on the surface of the torso

Note 1 to entry: The term sweat rate is also used as the physiological response of the human body to elevated metabolic rate and/or activity wearing protective clothing with high thermal insulation.

3.10
thermal human simulator measurement
THS
measurement with the sweating torso according to ISO 18640-1 where the device is coupled with a validated physiological model

Note 1 to entry: Test cases and requirements for the validation of the physiological model are provided in [A.3](#).

3.11

torso surface temperature

average temperature on the surface of the measurement area (0,43 m²) of the torso device

4 Symbols and abbreviations

For the purposes of this document the following symbols and abbreviated terms apply, in addition to the terms and definitions in ISO 18640-1.

C_{sk}	Wicking layer correction
E_{sk}	Skin diffusion
MAWD	Maximum allowable work duration (in minutes)
$T_{m,sk}$	Mean skin temperature in °C
T_{co}	Core body temperature in °C

5 Evaluation method

5.1 General

Physical parameters based on thermal properties of protective clothing resulting from standard torso measurements do not contain direct information about the thermo-physiological impact on the wearer for various firefighters' scenarios. Physiological data are deduced by doing measurements coupling sweating torso system to a physiological model as described in this document.

The results of these measurements are used to predict the maximum allowable work duration (MAWD) according to thermal characteristics and moisture management properties of the tested protective clothing system. This procedure was validated based on human subject trials (see [Annex A](#)).

5.2 Firefighting scenarios

Firefighters deal with a variety of tasks and challenges. Therefore, many scenarios have to be considered. In order to ensure a maximum level of comparability a moderate scenario has been defined which is applicable to a wide range of protective clothing inclusive of firefighting. The background and reasoning and the relevance for this standard are described in [Annex C](#).

5.2.1 Standard scenario for THS measurements

For the purpose of this standard a scenario was selected which reflects a moderate firefighter activity without fighting fire (see also [Annex C](#)).

The applied scenario is defined as follows:

- Ambient condition is set to 40 °C air temperature and 30 % RH;
- No radiation is present;
- Unidirectional wind speed of 1 m/s is applied;
- Physical activity is set to 6 Met²) (350 W/m² metabolic rate, which equals 285 W/m² metabolic heat production);
- Initial condition of the human body is assumed to be thermo-neutral ($T_{co} = 36,8$ °C; $T_{m,sk} = 34,2$ °C);

2) MET: Metabolic Equivalent of Task (1 MET = 1 kcal/(kg·h) = 4,184 kJ/(kg·h) alternatively 1 MET = 58,2 W/m²).